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THE UNITED STATES OF AMERICA

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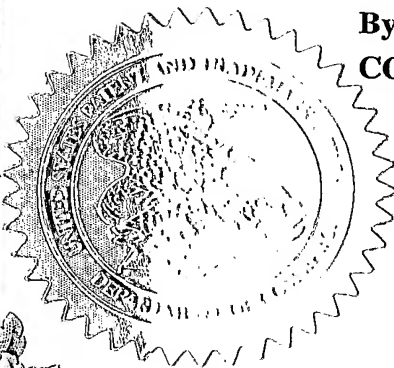
April 28, 2004

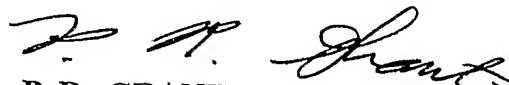
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APPLICATION NUMBER: 60/528,775

FILING DATE: December 12, 2003

By Authority of the
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PTO/SB/H6 (08-03)
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This is a request for filing a PROVISIONAL APPLICATION FOR PATENT under 37 CFR 1.53 (c).

INVENTOR(S)					
Given Name (first and middle [if any])		Family Name or Surname		Residence (City and either State or Foreign Country)	
Samuel Pedro		Goldman		Canada	
Jerry J.		Battista		Canada	
<input checked="" type="checkbox"/> Additional inventors are being named on the 1 separately numbered sheets attached hereto					
TITLE OF THE INVENTION (500 characters max)					
FAST INVERSE CASE OPTIMIZATION					
Direct all correspondence to: CORRESPONDENCE ADDRESS					
<input checked="" type="checkbox"/> Customer Number		1059			
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ENCLOSED APPLICATION PARTS (check all that apply)					
<input checked="" type="checkbox"/> Specification Number of Pages		8		<input type="checkbox"/> CD(s), Number	
<input type="checkbox"/> Drawing(s) Number of Sheets		<input type="checkbox"/> Other (specify)			
<input checked="" type="checkbox"/> Application Data Sheet. See 37 CFR 1.76					
METHOD OF PAYMENT OF FILING FEES FOR THIS PROVISIONAL APPLICATION FOR PATENT					
<input checked="" type="checkbox"/> Applicant claims small entity status. See 37 CFR 1.27.				FILING FEE AMOUNT (\$) 80.00	
<input type="checkbox"/> A check or money order is enclosed to cover the filing fees					
<input checked="" type="checkbox"/> The Director is hereby authorized to charge filing fees or credit any overpayment to Deposit Account Number: 022085					
<input type="checkbox"/> Payment by credit card. Form PTO-2038 is attached.					
The invention was made by an agency of the United States Government or under a contract with an agency of the United States Government.					
<input checked="" type="checkbox"/> No.					
<input type="checkbox"/> Yes, the name of the U.S. Government agency and the Government contract number are: _____					

Respectfully submitted,
 SIGNATURE

Timothy J. Sinnot

(Page 1 of 2)

Date

Dec.12/03

TYPED or PRINTED NAME

Timothy J. Sinnot

REGISTRATION NO.
(if appropriate)

31,083

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416-384-7311

Docket Number:

5611-35

USE ONLY FOR FILING A PROVISIONAL APPLICATION FOR PATENT
 This collection of information is required by 37 CFR 1.51. The information is required to obtain or retain a benefit by one public which is to file (and by the USPTO to process) an application. Confidentiality is governed by 35 U.S.C. 122 and 37 CFR 1.14. This collection is estimated to take 8 hours to complete, including gathering, preparing, and submitting the completed application form to the USPTO. Time will vary depending upon the individual case. Any comments on the amount of time you require to complete this form and/or suggestions for reducing this burden, should be sent to the Chief Information Officer, U.S. Patent and Trademark Office, U.S. Department of Commerce, P.O. Box 1450, Alexandria, VA 22313-1450. DO NOT SEND FEES OR COMPLETED FORMS TO THIS ADDRESS. SEND TO: Mail Stop Provisional Application, Correspondence for Patents, P.O. Box 1450, Alexandria, VA 22313-1450.

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Docket Number 9611-35		
INVENTOR(S)/APPLICANT(S)		
Given Name (first and middle (if any))	Family or Surname	Residence (City and either State or Foreign Country)
Jeff Z.	Chen	Canada

(Page 2 of 2)

Number 1 of 1

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FEE TRANSMITTAL for FY 2004 <small>Effective 10/01/2003. Patent fees are subject to annual revision.</small>	
<input checked="" type="checkbox"/> Applicant claims small entity status. See 37 CFR 1.27	
TOTAL AMOUNT OF PAYMENT	(\$) 80.00
Complete if known	
Application Number	
Filing Date	
First Named Inventor	Samuel Pedro Goldman
Examiner Name	
Art Unit	
Attorney Docket No.	9611-35

METHOD OF PAYMENT (check all that apply)		FEE CALCULATION (continued)																																																																																																																					
<input type="checkbox"/> Check <input type="checkbox"/> Credit card <input type="checkbox"/> Money Order <input type="checkbox"/> Other <input type="checkbox"/> None <input checked="" type="checkbox"/> Deposit Account: Deposit Account Number: 022095 Deposit Account Name: Bereskin & Parr The Director is authorized to: (check all that apply) <input type="checkbox"/> Charge fee(s) indicated below <input type="checkbox"/> Credit any overpayments <input checked="" type="checkbox"/> Charge any additional fee(s) or any underpayment of fee(s) <input type="checkbox"/> Charge fee(s) indicated below, except for the filing fee to the above-identified deposit account.		3. 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Signature		Date	December 12, 2003		

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Patent Application Data Sheet**Application Information****Application Type::** Provisional**Subject Matter::** Utility**Suggested****Classification::****Suggested Group Art****Unit::****Title::** FAST INVERSE DOSE OPTIMIZATION**Attorney Docket Number::** 9611-35**Request for Early****Publication?::** No**Request for Non-Publication?::** No**Suggested Drawing Figure::****Total Drawing Sheets::****Small Entity?::** Yes**Applicant Information****Inventor Authority Type::** Inventor**Primary Citizenship****Country::** Canadian**Status::** Full Capacity**Given Name::** Samuel**Middle Name::** Pedro

- 1 -

Initial 12/12/2003

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Status:: Full Capacity

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- 2 -

Initial 12/12/2003

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PATENT AND TRADEMARK OFFICE
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01 FC:2005 80.00 DA

PTO-1556
(5/87)

*U.S. Government Printing Office: 2002 — 489-267/69033

B&P File No. 9611-35

BERESKIN & PARR

UNITED STATES
PROVISIONAL APPLICATION

Title: Fast Inverse Dose Optimization

Inventors: Samuel Pedro Goldman, Jerry J. Battista and Jeff Z. Chen

FIDO - Fast Inverse Dose Optimization

Detailed Description of Invention

The most fundamental requirements of a radiation treatment optimization are: (i) dose is homogeneously deposited in the Planning Target Volume (PTV); (ii) the dose deposited in any Organ At Risk (OAR) does not exceed a threshold value and ideally should be zero; (iii) the dose deposited in All The Rest (ATR), i.e. organs and tissue not included in the PTV and OARs, should be as small as possible and ideally zero to minimize the risk of secondary carcinogenesis; (iv) the dose gradient crossing the PTV boundaries should be as high as possible. Optimizations are pursued by the minimization of a positive-definite objective function. A successful optimization will yield a global minimum to this objective function in a short computation time with physically achievable beamlet intensities.

This work presents a new approach to radiation treatment optimization that is very fast and yields a global minimum of the objective function without the use of a search routine but rather solves a linear system of equations. The possibility of such a direct optimization scheme has been known for decades but it has been impossible to implement rigorously using conventional quadratic objective functions because optimized results are only achievable with unphysical negative beamlet intensities [3]. Once an ad-hoc condition requiring the beamlet intensities to be positive is introduced (i.e. force negative values to be zero), the linear method yields a dose distribution with artefacts. Alternatively, one may pursue a minimum of the objective function by a direct search over all possible positive beam intensities, but this is a very time-consuming approach. In our work the negative-intensities problem is dealt with *within the objective function* and not as an externally imposed ad-hoc requirement.

We summarize now our approach. In the following we call "organ" any organ, target volume, region of tissue, identifiable anatomical entity or any defined volume within the volume exposed to radiation. For simplicity we will divide the set of organs into organs that must receive a certain dose and organs that should receive no dose or a dose as small as possible. A typical objective function O satisfying the optimization conditions stated above is of the form:

$$O = \sum_k \overset{\text{all organs with required dose}}{p_k^{dose} O_k^{dose}} + \sum_n \overset{\text{all organs without required dose}}{p_n^{no-dose} O_n^{no-dose}}$$

where the p_i are importance coefficients and the objectivity terms are:

$$O_k^{dose} = \sum_{x \in \text{organ } k} \left(\sum_i^{\text{all beamlets}} w_i d_i(x) - d^{orgk} \right)^2$$

$$O_n^{no-dose} = \sum_{x \in \text{organ } n} \left(\sum_i^{\text{all beamlets}} w_i d_i(x) \right)^2$$

where w_i is the weight of beamlet i , d_i is the dose deposited at destination point x by beamlet i and d^{orgk} is the dose required in organ k .

The main reason for the traditional appearance of negative weights upon optimization of the objective function O is the fact that we require satisfying two conflicting demands: on one hand we require $O^{ATR} = 0$ and on the other we require radiation to pass through the ATR (and possibly OARs) to reach the PTV. A correct requirement on O_{ATR} (and OARs) is that $O^{no-dose}$ should be minimized and $O^{no-dose}$ should be zero only if the weights of all the beamlets passing through the "no-dose" organs are zero. This requirement is satisfied if instead of that standard $O^{no-dose}$ above, we use new terms of the form

Detailed Description of Invention

$$\bar{O}_n^{no-does} = \sum_{\text{all organs}} \sum_{\text{all beamlets}} w_i^2 d_i^2(x)$$

****novel idea****

We have as well added another term to the objective function that replaces the unrealistic zero-limit for the beamlet weights with an equal-weight limit (cylindrical symmetry) which is usually the initial set of weights before optimization. This term is of the form

$$O^{sym} = \sum_i (w_i^2 - w_i).$$

****novel idea****

With the weights normalized to

$$\sum_i w_i = \text{total number of beamlets},$$

O^{sym} is positive and its minimum is zero when $w_i = 1$ for all i . O^{sym} provides the most powerful constraint to avoid negative weights.

With the new terms introduced above, the new objective function to be used is of the form:

$$O = \sum_n \sum_{\text{all organs with required data}} p_n^{does} O_n^{does} + \sum_n \sum_{\text{all organs without required data}} \bar{p}_n^{no-does} \bar{O}_n^{no-does} + p_{sym} O^{sym}$$

****novel idea****

Although not necessary (and in general counterproductive) the terms $O_n^{no-does}$ can also be added to the objective function. In our calculations, the terms $O_n^{no-does}$ were given non-zero importance coefficients when we wanted to demonstrate the appearance of negative weights upon optimization. With this consideration a more general objective function is:

$$O = \sum_n \sum_{\text{all organs with required data}} p_n^{does} O_n^{does} + \sum_n \sum_{\text{all organs without required data}} \bar{p}_n^{no-does} \bar{O}_n^{no-does} + p_{sym} O^{sym} + \sum_n \sum_{\text{all organs without required data}} p_n^{no-does} O_n^{no-does}$$

****novel idea****

Where the coefficients p_i are the importance parameters for organ s within an objectivity component and p_{sym} is the importance parameter of the asymptotic symmetry condition. The optimization problem for all the beam intensities is reduced to the solution of a linear system of equations as is shown in the following paragraphs.

The optimum of the objective function is obtained by minimizing the objective function from the system of equations:

The optimum of the positive-definite objective function O is obtained by minimizing O with respect to all the weights w_i . We perform this minimization by requiring the set of first derivatives of O to satisfy:

$$0 = \frac{\partial O}{\partial w_j} \quad \text{for all } w_j.$$

Consider the term O_n^{does} :

$$\frac{\partial O_n^{does}}{\partial w_j} = 2 \sum_{\text{all organs}} d_i(x) \left(\sum_i w_i d_i(x) - d^{sym} \right)$$

FIDO - Fast Inverse Data Optimization

Detailed Description of Invention

In our novel approach, we exchange the order of the summations to obtain:

$$\frac{\partial O_k^{dca}}{\partial w_j} = 2 \sum_i^{\text{all beamlets}} w_i \left(\sum_{x \in \text{array}_i} d_i(x) d_j(x) \right) - 2 d_i^{dca} \sum_{x \in \text{array}_j} d_j(x) \quad \text{novel idea}$$

This simple exchange in the summation order simplifies enormously the problem! We are now able to formulate the problem only in terms of the beamlet weights. The x -dependence (destination point dependence) has been eliminated by summing over all destination points *in advance*. We can define now the x -independent arrays:

$$\alpha_{ij}^{array_i} = \sum_{x \in \text{array}_i} d_i(x) d_j(x) \quad \text{novel idea}$$

and

$$\beta_j^{array_i} = d_i^{array_i} \sum_{x \in \text{array}_i} d_j(x) \quad \text{novel idea}$$

The optimization problem for the optimal weights w_i is given by the solution to the system of linear algebraic equations:

$$\sum_j^{\text{all beamlets}} \alpha_{ij} w_j = \beta_i \quad \text{novel idea}$$

where

$$\alpha_{ij} = \sum_b^{\text{all arrays with required data}} p_b^{dca} \alpha_{ij}^{array_b} + \sum_m^{\text{all arrays without required data}} p_m^{no-dca} \alpha_{ij}^{array_m} + \sum_n^{\text{all arrays without required data}} \bar{p}_n^{no-dca} \alpha_{ij}^{array_n} \delta_{ij} + p_{array} \delta_{ij} \quad \text{novel idea}$$

and

$$\beta_i = \sum_b^{\text{all arrays with required data}} p_b^{dca} \beta_i^{array_b} + \frac{1}{2} p_{array} \quad \text{novel idea}$$

The solution to the optimization problem is obtained by the numerical inversion of the matrix α_{ij} :

$$w_i = \sum_j^{\text{all beamlets}} \alpha_{ij}^{-1} \beta_j \quad \text{novel idea}$$

Fast Inverse Dose Optimization (FIDO) for IMRT via Matrix Inversion with no Negative Intensities

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Abstract

A fast optimization algorithm is very important for inverse planning of Intensity Modulated Radiation Therapy (IMRT), and for adaptive radiotherapy of the future. Conventional numerical search algorithms such as the conjugate gradient search, conducted with positive beam weight constraints, generally require many iterations and may produce suboptimal results due to trapping in local minima. A direct solution of the inverse problem using conventional quadratic objective functions without positive beam constraints is more efficient but will result in unrealistic negative beam weights. We present here a direct solution of the inverse problem which does not result in unacceptable negative beam weights. The objective function for the optimization of beam intensities for large number of beamlets is reformulated such that the optimization problem is reduced to a linear set of equations. The optimal set of intensities is found through a matrix inversion, and negative beamlet intensities are avoided without the need for externally imposed constraints. The method has been applied to a test phantom and to a few clinical cases. We were able to achieve highly conformal dose distributions with very short optimization times. Typical optimization times for a single anatomical slice using a single processor desktop computer are: 0.2 sec. for 400 beamlets; 8 sec. for 1,000 beamlets; 40 sec. for 2,000 beamlets and 2.5 min for 3,000 beamlets. These times can be substantially further improved using a better optimization routine for matrix inversion. In conclusion, the new method provides a fast and robust technique to find a global minimum that yields excellent results for the inverse planning of IMRT.

Keywords

Inverse planning, optimization, objective function.

Introduction

Intensity Modulated Radiation Therapy (IMRT) is becoming a new standard for radiotherapy. Given the better conformal dose distributions obtained through IMRT and its dynamic delivery features, adaptive radiotherapy becomes an important factor to be considered. A fast optimization algorithm is crucial not only for designing good radiation treatment plans but also for the successful implementation of future interactive adaptive treatment techniques. Conventional optimization algorithms using numerical searches such as the conjugate gradient search [1-2] with positive beam weight constraints usually require many iterations (i.e. long computation times) and may result in suboptimal plans due to trapping in local minima of the objective function. A direct solution of the inverse problem using conventional quadratic objective functions without imposing positive beam constraints will be computationally faster but will result in unrealistic negative beam weights. We present here a very fast method for the direct solution of the inverse problem (FIDO) that avoids the difficulty of negative beam weights and preserves efficiency.

Method

The most fundamental requirements of a radiation treatment optimization are: (i) dose is homogeneously deposited in the Planning Target Volume (PTV); (ii) the dose deposited in any Organ At Risk (OAR) does not exceed a threshold value and

ideally should be zero; (iii) the dose deposited in All The Rest (ATR), i.e. organs and tissue not included in the PTV and OARs, should be as small as possible and ideally zero to minimize the risk of secondary carcinogenesis; (iv) the dose gradient crossing the PTV boundaries should be as high as possible. Optimizations are pursued by the minimization of a positive-definite objective function. A successful optimization will yield a global minimum to this objective function in a short computation time with physically achievable beamlet intensities.

This work presents a new approach to radiation treatment optimization that is very fast and yields a global minimum of the objective function without the use of a search routine but rather solves a linear system of equations. The possibility of such a direct optimization scheme has been known for decades but it has been impossible to implement rigorously using conventional quadratic objective functions because optimized results are only achievable with unphysical negative beamlet intensities [3]. Once an ad-hoc condition requiring the beamlet intensities to be positive is introduced (i.e. force negative values to be zero), the linear method yields a dose distribution with artefacts. Alternatively, one may pursue a minimum of the objective function by a direct search over all possible positive beam intensities, but this is a very time-consuming approach. In our work the negative-intensities problem is dealt with *within the objective function* and not as an externally imposed ad-hoc requirement.

We summarize now our approach. For simplicity we will consider a single PTV, a single OAR and a single ATR. A typical objective function O satisfying the optimization conditions stated above is of the form:

$$O = p_{PTV} O_{PTV} + p_{OAR} O_{OAR} + p_{ATR} O_{ATR}$$

where the p_i are importance coefficients and the objectivity terms are:

$$O_{PTV} = \sum_{x \in PTV} \left(\sum_i^{all\ beamlets} w_i d_i(x) - d^{PTV} \right)^2,$$

$$O_{OAR} = \sum_{x \in OAR} \left(\sum_i^{all\ beamlets} w_i d_i(x) \right)^2,$$

and $O_{ATR} = \sum_{x \in ATR} \left(\sum_i^{all\ beamlets} w_i d_i(x) \right)^2,$

where w_i is the weight of beamlet i , d_i is the dose deposited at destination point x by beamlet i and d^{PTV} is the dose prescribed to the PTV. The main reason for the traditional appearance of negative weights upon optimization of the objective function O is the fact that we require satisfying two conflicting demands: on one hand we require $O_{ATR} = 0$ and on the other we require radiation to pass through the ATR (and possibly OARs) to reach the PTV. A correct requirement on O_{ATR} is that O_{ATR} should be minimized and O_{ATR} should be zero only if the weights of all the beamlets passing through the ATR are zero. This requirement is satisfied if instead of O_{ATR} we use a new ATR term of the form

$$\bar{O}_{ATR} = \sum_{x \in ATR} \sum_i^{all\ beamlets} w_i^2 d_i^2(x).$$

Similarly for the OAR we use:

$$\bar{O}_{OAR} = \sum_{x \in OAR} \sum_i^{all\ beamlets} w_i^2 d_i^2(x).$$

We have as well added another term to the objective function that replaces the unrealistic zero-limit for the beamlet weights with an equal-weight limit (cylindrical symmetry) which is usually the initial set of weights before optimization. This term is of the form

$$O_{eqm} = \sum_i^{all\ beamlets} (w_i^2 - w_i).$$

With the weights normalized to

$$\sum_i^{all\ beamlets} w_i = \text{total number of beamlets},$$

O_{eqm} is positive and its minimum is zero when $w_i = 1$ for all i .

With these modifications, the optimization problem for all the beam intensities is reduced again to the solution of a linear system of equations of the form:

$$\sum_j \alpha_{ij} w_j = \beta_i \quad (1)$$

where w_j is the (unknown) weight or intensity of beamlet j , β_i is a vector of coefficients that depends on the dose deposited by beam i within the PTV, and α_{ij} is a matrix that describes the product of the doses deposited by the intersecting pairs of beamlets i and j on different organs (each organ with its importance coefficient). The set of optimal beam weights is obtained from (1) by inversion:

$$w_i = \sum_j \alpha_{ij}^{-1} \beta_j,$$

In other words, the solution to the (large) system of linear equations (1) is obtained quickly and accurately by inverting the array α_{ij} using standard matrix inversion routines.

Results

Below we present several sets of preliminary results obtained with this technique for a prostate case, a head and neck case, and an "interlocked rectangles" phantom on a 2D slice. Only primary KERMA has been included in the calculations reported here, but very similar results are obtained in dose distributions, when the calculated beam intensities are imported to a commercial treatment planning system (Theraplan Plus V3.8, Nucletron). The only difference is a slightly diffused dose to the OARs due to scatter spreading effects. In each case, we include calculation and optimization times for KERMA calculations as they were obtained on a single-processor desktop PC. The program was written in C# using the Microsoft .NET environment. The matrix inversion routine was obtained from *Numerical Recipes* [4] and translated from FORTRAN into C#. No effort has been devoted to maximize the speed of the matrix inversion procedure.

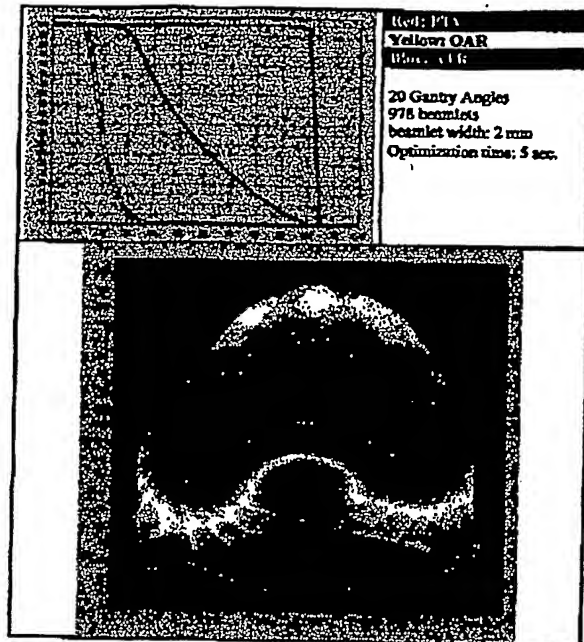
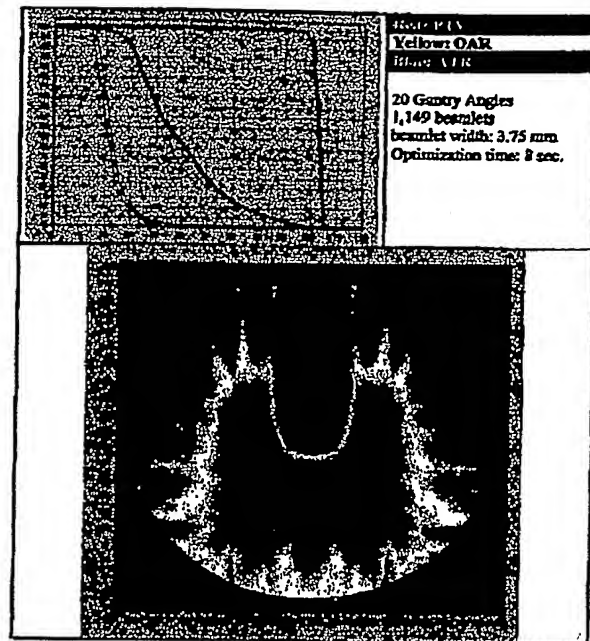
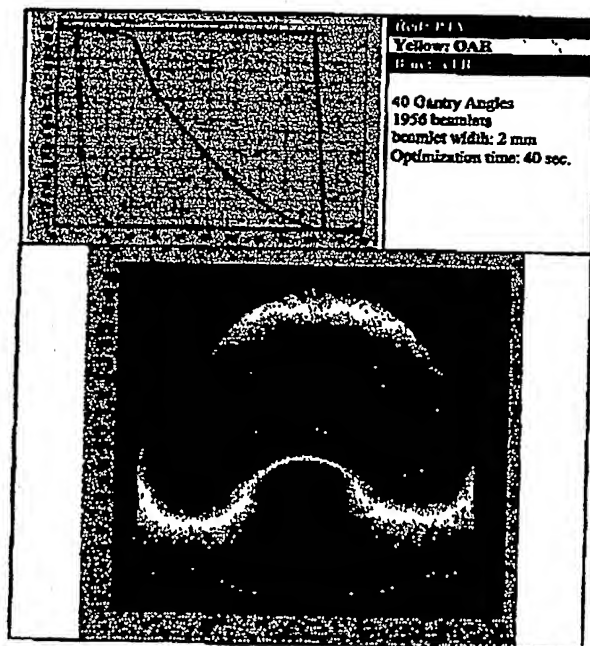
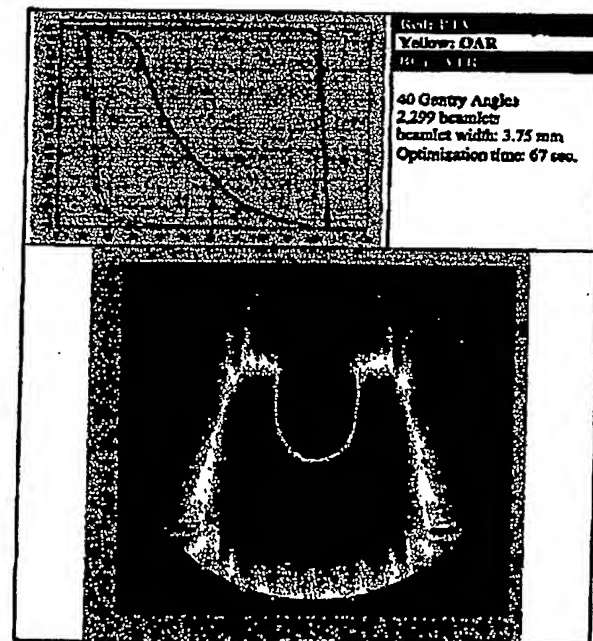
In all cases the number of gantry angles used is evenly distributed over a full 360 degree circle around the isocentre. Each beam is evenly divided into beamlets of the specified width resulting in the total number of beamlets quoted. The source to axis distance (SAD) is 100 cm. In each case we also present the DVH, scaled to 100% volume on the vertical axis and 100% dose on the horizontal axis, and a colour-coded dose deposition map with blue showing no dose deposition (primary KERMA only) and red the largest dose deposition.

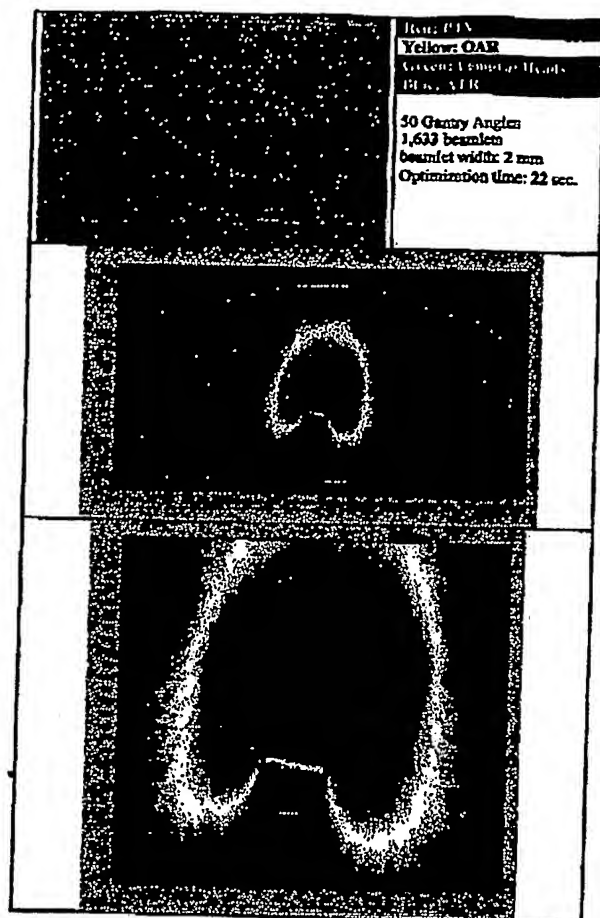
Conclusions and future work

We have developed a fast and robust technique to find a global minimum that yields excellent results for the inverse optimization problem for the radiation treatment of tumours, using large sets of non-negative intensity-modulated beamlets.

Work is currently in progress on a full implementation FIDO in our treatment planning system that uses collapsed cone convolution method for dose calculation [5]. Work is proceeding as well on an efficient 3D implementation for on-line adaptive radiotherapy as might be possible with helical tomotherapy [6].

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Figure 1: Head and Neck Case. - 20 gantry angles**Figure 3: Interlocked Rectangles Phantom. - 20 gantry angles****Figure 2: Head and Neck Case. - 40 gantry angles****Set No. 4: Interlocked Rectangles. - 40 gantry angles**

Set No. 5: Prostate Case (Panoramic and close-up views).**References**

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We claim:

1. A method for optimizing radiation treatment, said method comprising the step of resolving an objective function, said objective function comprising importance coefficients and objectivity terms.
2. A system for optimizing radiation treatment, said system comprising means for resolving an objective function.
3. A method of planning delivery of radiation therapy to maximize radiation to a planned target volume and minimize radiation to surrounding tissues outside the planned target volume, said method comprising the step of resolving an objective function.
4. The invention substantially as described and illustrated herein.